Structural Analysis Report

Date: 09.05.2021

Boat: Tanaruz 7.5m – (Longitudinal Structure)

1- Input Data

This document includes the structural calculations of the Tanaruz-S 7.5 meters boat. To perform the calculations "Strength Model Tanaruz S 7.5m – Longitudinal Structure.3dm" file is used. In the calculations, three different cases are simulated as sea conditions, and analyses were performed following the same procedure for all calculations. Tanaruz S boat is 7.5 meters in length and wave function is created based on the length of the boat.

The sinusoidal wave assumption is used in the analysis as shown in Figure 1. The sinusoidal wave assumption allows creating wave crest and wave through conditions for a hull.



Figure 1 - Wave Assumption

For Tanaruz S which has 7.5-meter length, sinusoidal wave function creates 375mm wave height and 7500mm wavelength in order to provide the crest and trough conditions. In the following chapters, wave conditions are detailed.

FGF PP Glassfiber (30%) is used as material for the Tanaruz S structural analysis.

Material properties		
Description	Testmethod	Typical value
Specific gravity	ISO 1183	1,12 g/cc
MFI 230°C/2,16 kg	ISO 1133	13 g/10min
Tensile Strength at Yield	ISO 527	90 MPa
Elongation-Strain at Break	ISO 527	5%
Tensile modulus	ISO 527	7500 Mpa
Impact strength - Charpy method notched 23°C	ISO 179	10 kJ/m ²
Impact strength – Izod method notched 23°C	ISO 180	10 kJ/m ²
Flexural modulus	ISO 178	5900 MPa
Vicat softening temperature A	ISO 306	166°C
Vicat softening temperature B	ISO 306	140°C
Heat deflection temperature A 1,8 MPa	ISO 75	150°C
Heat deflection temperature B 0,45 MPa	ISO 75	161°C

Figure 2 - FGF PP Glassfiber Mechanical Properties

2- Model

The file "Strength Model Tanaruz S 7.5m – Longitudinal Structure.3dm" which is used to perform the structural analysis includes the 3D model of the boat. Figure 3 shows the 3D view of the Tanaruz-S file used for analysis.



Figure 3 - 3D View of Tanaruz-S 7.5m

"Strength Model Tanaruz S 7.5m.3dm" file includes 7 poly-surfaces and the mentioned poly-surfaces are shown in Figure 4. All of the poly-surfaces are checked and noted that all of them are valid and acceptable to use in structural calculations. Tanaruz 7.5 meters model is created by extending the 4.5 meter model and transverse beams are removed from the geometry on the forward side of the bulkhead. Only one tranverse is kept on the hull and this tranverse works as a ring frame because one of the tranverse beam on the super-structure is also kept which is in the same section with the hull bottom transverse. Therefore, by connecting these transverse beams (hull transverse and superstructure beam), a whole ring frame is created.



3- Calculation Method and Cases

In order to calculate the total weight value and to establish the loads on the boat, the "WeightDistribution Tanaruz S.xlsx" file is used. The file contains the weights of the components on the boat and the shared file shows the locations of the components additionally. Figure 5 shows a sample part of the weight distribution file. Tanaruz 4.5 m model was extended to 7.5 meters by keeping the thickness and longitudinal structure as mentioned. Additional boat weight is added into the total weight of Tanaruz4.5meters including all the extended surfaces which are hull, hull structure, deck and super structure of the boat.

								POSITION		comment
Basic			optional							
equipment			equipment	pcs.	weight (kg)	Full weight	X (m)	Y (m)	Z (m)	
	2	BILGE PUMP		2	2	4	2	0	0.35	
	3	16A/230V RATIO SHOREPOWER CONNECTOR		1	0.5	0.5	-0.1	0.5	0.7	
	2 810 3 116 4 ch 6 Fu 7 MM 8 W 9 811 10 67 11 An 12 wr 13 AN 14 An 14 An 15 All 16 Co 17 Es 18 ho 19 ba	charging cable, 10 m		1	4	4	0.5	0.6	0.35	(in the sit) PS
	6	Fusion MS-DAB100A DAB+ module, incl. antenne		1	2	2	2	0	1.8	
	7	Marine RADIO		1	0.3	0.3	2	0.6	1.4	
	8	WI-Fi Antenne (client choice)		0		0				
	9	Bluetoth Antenne (client choice)		0		0				
	Deficient Antenne (client choice) Of Sa Antenne (client choice) Archoring rose Jonn Archor lang Jonn Archor holding Archor holding			0		0				
				1	3	3	0.5	-0.6	0.35	(in the sit) SB
				0		0				
	13	ANCHOR 10kg		0		10	4	0	1.05	
	14	Anchor holding		1	1	1	4.5	0	1.25	
Exterior										
Exterior	15	Aluminium Side window		2	15	30	3	0	1.4	
	16	Companionway door		1	15	15	2	0	1	
	17	Escape top HATCH SOVED CM		1	2	2	9.1	0	1.6	
	18	holding systems for access to find tanks	+ +	2	0.5	1	3.5	0	0.55	
	19	hatches (acess system) to the hattery compartment		1	3	3	1.5	0	0.4	
	20	CHROMIUM HANDRAILS 32X1400mm		4	5	20	2	0	1.2	
	20	clast (kikkar) 30MM 55 X 200 X 70MM		4	0.7	2.8	3	0	1.2	
	22	TELESKOPIC ledder 4 stens SLE44	+ +	0	3	0	3	0		
	22	RIOWER (westilation in 8 out)		2	0.6	12	2	0	1	
	2.0	Audo signal system (whistler	-	4	0.0	0	~	0		
	25	Solar papeals	+ +	1	4	4	2.5	0.6	1.2	
	25	solar panies	-	1	15	1.6	3.5	-0.6	1.2	
	20	solar panel caster (cast up entions)		-	1	1	3	0.6	1.4	
	21	solar paner control (see two options)	-	1	1		2	0.0	1.4	
Inner			-							
Lamps	20	10 200/ 7W Jatasias Lama	-	4	0.2	0.0		0	1.5	
	20	Extend long and light		4	0.2	0.8	3	0	1.5	
	29	201 112 E and land automatic accounting 1200 white		2	0.2	0.4	2.2	0	1.5	
-	30	12V - 112,5 reu lamp external + green + writte + 360 Write	-	4	0.35	1.4	2.2	0	1.9	
Switcher										
Switches	21	NUCTOON ENERGY BULLE CHART (DC2) CHARCED 12/05	-		1		2	0.0	0.2	
-	21	Catalalananal		1	1	1	2	-0.0	0.2	
	32	Ischakeipaneei		1	0.4	0.4	2	0.6	0.8	

Figure 5 - Weight Distribution File

The total weight is 2070 kgs and this is equal to 2019.5 m₃ displacement volume for the defined load condition.

As shown in Figure 6, all of the weights are distributed on the boat in the 3D modeling software first. This method provides an opportunity to observe the weight distribution in the 3D model and to determine the loading surfaces of the weights on the boat.



Figure 6 - 3D View of Weight Distribution

After calculating the total weight on the boat, displacement volume and water-plane are determined. Figure 7 shows the draught and displacement of Tanaruz S at the defined loading condition which equals to 2070kgs.



Figure 7 - Displacement of the Hull 2070kgs

To create the wave function and to calculate the hydrostatic pressure load on the hull, the Tanaruz S7.5 hull is split into 100 virtual sections which have 75mm spacing. Figure 8 shows the section spacing view defined on the hull.



Figure 8 - Wave Function and Hydrostatic Pressure Spacing

Figure 9 shows the wave function as a curve for wave crest condition. The figure provides a visulation of the wave function which was used for the structural analysis.



Figure 9 - Wave Function and Hydrostatic Pressure Spacing

Keel and still water level coordinates are determined and with the help of these values, still water hydrostatic pressures are calculated. By using the sinusoidal wave function, wave crest and wave trough distribution are determined for every 100 sections. Still water, wave trough, and wave crest pressure values and wave coordinates are shown in Figure 10 partially.

Hull Keel	Still Water	Wave Crest	Wave Troug	gh	Still Water Load	Wave Crest Load		Wave Trough Load
X Y Keel	s x keel-Z Pressure	s x wave-Z keel-Z difference Pressure	s wave-Z keel-Z	difference Pressure	0 0 0	0 0 0 -112.5000	0	0 0 112.5000 0
0 0 -95.14	0 0 -95.1400 956.6565	0 0 -112.5000 -95.1400 -17.3600 0.0000	0 0 112.5000 -95.1400	207.6400 2087.8721	50 0 0	0 50 0 -112.2260	0	50 0 112.2260 0
50 0 -102.88	1 50 -102.8800 1034.4841	1 50 -112.2260 -102.8800 -9.3460 0.0000	1 50 112.2260 -102.8800	215.1060 2162.9442	100 0 0	0 100 0 -111.4052	0 1	00 0 111.4052 0
100 0 -110.59	2 100 -110.5900 1112.0101	2 100 -111.4052 -110.5900 -0.8152 0.0000	2 100 111.4052 -110.5900	221.9952 2232.2168	150 0 0	0 150 0 -110.0416	0 1	50 0 110.0416 0
150 0 -118.26	3 150 -118.2600 1189.1339	3 150 -110.0416 -118.2600 8.2184 82.6380	3 150 110.0416 -118.2600	228.3016 2295.6297	200 0 0	0 200 0 -108.1419	0 2	00 0 108.1419 0
200 0 -125.89	4 200 -125.8900 1265.8554	4 200 -108.1419 -125.8900 17.7481 178.4612	4 200 108.1419 -125.8900	234.0319 2353.2497	250 0 0	0 250 0 -105.7154	0 2	50 0 105.7154 0
250 0 -133.47	5 250 -133.4700 1342.0742	5 250 -105.7154 -133.4700 27.7546 279.0792	5 250 105.7154 -133.4700	239.1854 2405.0692	300 0 0	0 300 0 -102.7739	0 3	00 0 102.7739 0
300 0 -141.00	6 300 -141.0000 1417.7903	6 300 -102.7739 -141.0000 38.2261 384.3734	6 300 102.7739 -141.0000	243.7739 2451.2071	350 0 0	0 350 0 -99.3316	0 3	50 0 99.3316 0
350 0 -148.47	7 350 -148.4700 1492.9030	7 350 -99.3316 -148.4700 49.1384 494.0989	7 350 99.3316 -148.4700	247.8016 2491.7071	400 0 0	0 400 0 -95.4054	0 4	00 0 95.4054 0
400 0 -155.87	8 400 -155.8700 1567.3118	8 400 -95.4054 -155.8700 60.4646 607.9866	8 400 95.4054 -155.8700	251.2754 2526.6371	450 0 0	0 450 0 -91.0144	0 4	50 0 91.0144 0
450 0 -163.18	9 450 -163.1800 1640.8157	9 450 -91.0144 -163.1800 72.1656 725.6430	9 450 91.0144 -163.1800	254.1944 2555.9884	500 0 0	0 500 0 -86.1800	0 5	00 0 86.1800 0
500 0 -170.39	10 500 -170.3900 1713.3140	10 500 -86.1800 -170.3900 84.2100 846.7526	10 500 86.1800 -170.3900	256.5700 2579.8755	550 0 0	0 550 0 -80.9257	0 5	50 0 80.9257 0
550 0 -177.49	11 550 -177.4900 1784.7063	11 550 -80.9257 -177.4900 96.5643 970.9779	11 550 80.9257 -177.4900	258.4157 2598.4347	600 0 0	0 600 0 -75.2772	0 6	00 0 75.2772 0
600 0 -184.46	12 600 -184.4600 1854.7914	12 600 -75.2772 -184.4600 109.1828 1097.8604	12 600 75.2772 -184.4600	259.7372 2611.7224	650 0 0	0 650 0 -69.2619	0 6	50 0 69.2619 0
650 0 -191.26	13 650 -191.2600 1923.1671	13 650 -69.2619 -191.2600 121.9981 1226.7212	13 650 69.2619 -191.2600	260.5219 2619.6130	700 0 0	0 700 0 -62.9092	0 7	00 0 62.9092 0
700 0 -197.89	14 700 -197.8900 1989.8334	14 700 -62.9092 -197.8900 134.9808 1357.2657	14 700 62.9092 -197.8900	260.7992 2622.4012	750 0 0	0 750 0 -56.2500	0 7	50 0 56.2500 0
750 0 -204.30	15 750 -204.3000 2054.2876	15 750 -56.2500 -204.3000 148.0500 1488.6798	15 750 56.2500 -204.3000	260.5500 2619.8954	800 0 0	0 800 0 -49.3168	0 8	00 0 49.3168 0
800 0 -210.45	16 800 -210.4500 2116.1274	16 800 -49.3168 -210.4500 161.1332 1620.2351	16 800 49.3168 -210.4500	259.7668 2612.0197	850 0 0	0 850 0 -42.1432	0 8	50 0 42.1432 0
850 0 -216.32	17 850 -216.3200 2175.1517	17 850 -42.1432 -216.3200 174.1768 1751.3908	17 850 42.1432 -216.3200	258.4632 2598.9125	900 0 0	0 900 0 -34.7644	0 9	00 0 34.7644 0
900 0 -221.87	18 900 -221.8700 2230.9583	18 900 -34.7644 -221.8700 187.1056 1881.3935	18 900 34.7644 -221.8700	256.6344 2580.5232	950 0 0	0 950 0 -27.2162	0 9	50 0 27.2162 0
950 0 -227.06	19 950 -227.0600 2283.1451	19 950 -27.2162 -227.0600 199.8438 2009.4792	19 950 27.2162 -227.0600	254.2762 2556.8109	1000 0 0	0 1000 0 -19.5354	0 10	00 0 19.5354 0
1000 0 -231.88	20 1000 -231.8800 2331.6114	20 1000 -19.5354 -231.8800 212.3446 2135.1778	20 1000 19.5354 -231.8800	251.4154 2528.0449	1050 0 0	0 1050 0 -11.7595	0 10	50 0 11.7595 0
1050 0 -236.31	21 1050 -236.3100 2376.1561	21 1050 -11.7595 -236.3100 224.5505 2257.9119	21 1050 11.7595 -236.3100	248.0695 2494.4004	1100 0 0	0 1100 0 -3.9262	0 11	00 0 3.9262 0
1100 0 -240.36	22 1100 -240.3600 2416.8799	22 1100 -3.9262 -240.3600 236.4338 2377.4010	22 1100 3.9262 -240.3600	244.2862 2456.3587	1150 0 0	0 1150 0 3.9262	0 11	50 0 -3.9262 0
1150 0 -244.02	23 1150 -244.0200 2453.6821	23 1150 3.9262 -244.0200 247.9462 2493.1610	23 1150 -3.9262 -244.0200	240.0938 2414.2032	1200 0 0	0 1200 0 11.7595	0 12	00 0 -11.7595 0
1200 0 -247.31	24 1200 -247.3100 2486.7639	24 1200 11.7595 -247.3100 259.0695 2605.0081	24 1200 -11.7595 -247.3100	235.5505 2368.5196	1250 0 0	0 1250 0 19.5354	0 12	50 0 -19.5354 0
1250 0 -250.22	25 1250 -250.2200 2516.0247	25 1250 19.5354 -250.2200 269.7554 2712.4582	25 1250 -19.5354 -250.2200	230.6846 2319.5911	1300 0 0	0 1300 0 27.2162	0 13	00 0 -27.2162 0
1300 0 -252.76	26 1300 -252.7600 2541.5650	26 1300 27.2162 -252.7600 279.9762 2815.2308	26 1300 -27.2162 -252.7600	225.5438 2267.8992	1350 0 0	0 1350 0 34.7644	0 13	50 0 -34.7644 0
1350 0 -254.93	27 1350 -254.9300 2563.3849	27 1350 34.7644 -254.9300 289.6944 2912.9497	27 1350 -34.7644 -254.9300	220.1656 2213.8200	1400 0 0	0 1400 0 42.1432	0 14	00 0 -42.1432 0
1400 0 -256.77	28 1400 -256.7700 2581.8865	28 1400 42.1432 -256.7700 298.9132 3005.6474	28 1400 -42.1432 -256.7700	214.6268 2158.1257	1450 0 0	0 1450 0 49.3168	0 14	50 0 -49.3168 0
1450 0 -258.30	29 1450 -258.3000 2597.2711	29 1450 49.3168 -258.3000 307.6168 3093.1634	29 1450 -49.3168 -258.3000	208.9832 2101.3788	1500 0 0	0 1500 0 56.2500	0 15	00 0 -56.2500 0
1500 0 -259.58	30 1500 -259.5800 2610.1418	30 1500 56.2500 -259.5800 315.8300 3175.7496	30 1500 -56.2500 -259.5800	203.3300 2044.5340	1550 0 0	0 1550 0 62.9092	0 15	50 0 -62.9092 0
1550 0 -260.57	31 1550 -260.5700 2620.0965	31 1550 62.9092 -260.5700 323.4792 3252.6642	31 1550 -62.9092 -260.5700	197.6608 1987.5287	1600 0 0	0 1600 0 69.2619	0 16	00 0 -69.2619 0
1600 0 -261.23	32 1600 -261.2300 2626.7330	32 1600 69.2619 -261.2300 330.4919 3323.1788	32 1600 -69.2619 -261.2300	191.9681 1930.2871	1650 0 0	0 1650 0 75.2772	0 16	50 0 -75.2772 0
1650 0 -261.52	33 1650 -261.5200 2629.6490	33 1650 75.2772 -261.5200 336.7972 3386.5800	33 1650 -75.2772 -261.5200	186.2428 1872.7180	1700 0 0	0 1700 0 80.9257	0 17	00 0 -80.9257 0
1700 0 -261.57	34 1700 -261.5700 2630.1517	34 1700 80.9257 -261.5700 342.4957 3443.8802	34 1700 -80.9257 -261.5700	180.6443 1816.4233	1750 0 0	0 1750 0 86.1800	0 17	50 0 -86.1800 0
1750 0 -261.57	35 1750 -261.5700 2630.1517	35 1750 86.1800 -261.5700 347.7500 3496.7132	35 1750 -86.1800 -261.5700	175.3900 1763.5903	1800 0 0	0 1800 0 91.0144	0 18	00 0 -91.0144 0
1800 0 -261.57	36 1800 -261.5700 2630.1517	36 1800 91.0144 -261.5700 352.5844 3545.3244	36 1800 -91.0144 -261.5700	170.5556 1714.9791	1850 0 0	0 1850 0 95.4054	0 18	50 0 -95.4054 0
1850 0 -261.57	37 1850 -261.5700 2630.1517	37 1850 95.4054 -261.5700 356.9754 3589.4770	37 1850 -95.4054 -261.5700	166.1646 1670.8265	1900 0 0	0 1900 0 99.3316	0 19	00 0 -99.3316 0
1900 0 -261.57	38 1900 -261.5700 2630.1517	38 1900 99.3316 -261.5700 360.9016 3628.9559	38 1900 -99.3316 -261.5700	162.2384 1631.3476	1950 0 0	0 1950 0 102.7739	0 19	50 0 -102.7739 0

Figure 6 - A Partial View of the Wave Fuctions and Loads

Mesh is created in the structural analysis software as shown in Figure 11 and Figure 12. Mesh file includes 7 poly-surfaces which are meshed according to the mesh quality criteria of the software. All of the poly-surfaces mesh as a separate solid but in the calculations, these poly-surfaces are calculated as structurally bonded.



Figure 7 - Mesh View



Figure 12 - Mesh View (Hull Structure)

Figures 13, 14, and 15 show the hydrostatic pressure distribution on the hull. There are three calculation cases mentioned in the "Input Data" section. Wave crest and wave trough are the worst cases for a conventional displacement hull. (There may be slamming cases for a boat in extreme weather conditions. The calculations which are detailed in this report do not include any dynamic and time-dependent cases such as slamming..etc.)



The figure above shows three cases as a sample and the following pictures show these cases as hydrostatic pressure distribution on Tanaruz S 7.5meters hull.



Figure 8 - Still Water Hydrostatic Pressure



Figure 14 - Wave Crest Hydrostatic Pressure



Figure 15 - Wave Trough Hydrostatic Pressure

Weights are defined as forces to the boat on the related surfaces which are shown in the previous section. Figure 16 shows the weight distribution applied to the structural model.



Figure 16 - Weigth Distribution on Structural Model

After defining all of the loads on the boat analyze can be solved. But there should be a fixed point to perform the analysis. In real conditions, ships have not a fixed point. Ships stay on the see free surface freely. In such cases "Inertia Relief" method is used. Water pressure acts as a support for the boat. The applied loads and hull weight which is simulated with gravity work against the hydrostatic pressure. The technique of inertia relief has been a well-known approach for the analysis of unsupported systems such as air vehicles in flight, sea vehicles on the sea, automotive in motion, or satellites in space.

4- Results

The following figures show the stress and deformation distribution on Tanaruz 7.5 meters for each condition defined. If all of the plots are inspected carefully, it can be stated that maximum stress value is observed at the wave trough condition which is 10.58Mpa. Maximum stress value on the hull structure is below the yield stress value of FGF PP Glass-fiber which is 90Mpa. But deflections on the boat structure is an important point that maximum deflection value should be below the allowable deflections.

Maximum deflection is observed on the hull bottom between the longitudinals. Maximum deflection is 7.32mm where the maximum allowable deflection is 8mm (2% of the panel span). It can be stated

that the created structure is in the safe zone stresswise but very close to deflection limit. In conclusion, Tanaruz 7.5 meters longitudinal based structure satisfies the stress and deflection requirements, and also structure is in a well-balanced point that as deflection values shows, boat structure in not a heavy design.



Figure 17 - Still Water Stress Plot Section View



Figure 9 - Still Water Deformation Plot



Figure 10 - Wave Crest Stress Plot Section View



Figure 20 - Wave Crest Deformation Plot



Figure 21 - Wave Trough Stress Plot Section View



Figure 22 - Wave Trough Deformation Plot